9

Title Page

Vibration Diagnostic of Rotor Mechanisms in Ships



This Thesis was submitted to the Department of Mechanical Engineering of the University of Moratuwa on the in partial fulfillment of the requirements for the Degree of Master of Philosophy.



621 "01" 624.5.015.5

Department of Mechanical Engineering, University of Moratuwa, Sri Lanka. November, 2001.

74-4-4.1

TH

Declaration

Here with, I certify that the work included in the Thesis in part or whole, has not been submitted for any other academic qualification at any institution.

UOM Verified Signature

UOM Verified Signature

GG. Jayarathne (Candidate)

Dr. P.A.B.A.R. Perera (Supervisor)



ABSTRACT

In ships, there are so many sources of noise and Vibration such as propulsion engines and electric generators in restricted spaces and structures of ships, which are made of steel, transmit vibration well. By the reasons, noise and vibration of ships are very big by nature and reduction of noise and vibration is important subject for ships. Regarding noise reduction, reduction of noise cause by vibration has difficulty and the major part of such noise is structure born noise.

"Vibration" is not a problem. It is a physical manifestation of machinery imperfection. It is used to help find obvious and subtle deviations in machines. No machine runs perfect. "Diagnosis" is the Method of Detection. If, a fault develops and goes undetected, then, at best, the problem will not be too serious and can be remedied quickly and cheaply; at worst, it may result in expensive damage and down-time, injury, or even loss of life. There is no reason or excuse to have machinery operate unprotected. The areas of interest in vibration measuring in plant maintenance are general measurement, analysis, and corrective.

All rotor mechanisms in ships consist of shafts, bearings, couplings, gears etc. These machinery operate under various load conditions from light to heavy. Ship propulsion system comparatively works under very heavy load conditions with rolling and pitching of the ship which may tend to cause overstressing of shafts.

Objective of the Research: University of Moratuwa, Sri Lanka.

The aim of the project is to identify the vibration analysis of a ship transmission system. A ship transmission system is the link between the crank shaft (or thrust block) end and the propeller of the vessel. As it contains number of shafts, couplings and bearings it tends to cause severe vibrations due to various running and incipient defects. These defects can be diagnosed by measuring the level of vibration to the extent they excited.

Methodology Adopted: A Test Rig:

The test rig is a model of the transmission system of the ship "M/V Lanka Mahapola" made in to a scale of 1:10. Level and condition of lubrication maintained. Accelerometers are mounted over the bearing casings to trace the excitement of individual bearings.

Diagnosis of the misaligned and unbalanced shafts and defected sleeve (fluid film) bearings are done by using the "AUTOVIB" software package which is a vibration monitoring method introduce by this project.

Final Outcome of this research:

Although spectrum analysis method is not in use, similar demodulation techniques, will be practical, for the diagnostics of Sleeve (Fluid Film) bearings.

Measurement of the vibrations excited by bearing friction forces present all the necessary information for Diagnostics of bearing condition including installation problems and the quality of lubrication.

ACKNOWLEDGEMENT

I'd like to give special thanks to Dr. T.A. Piyasiri, Director/ITUM, who encouraged me for a M.Phil. Big tip of the hat to Dr. Piyasiri, for his help and valuable suggestions given.

A special thanks goes to Prof. P.A.de Silva, Ex. Head/Mechanical Engineering, for his grateful effort and valuable advices to make this success.

This project wouldn't have been possible without the concerted effort (on importing Vibration measuring equipment) of Former Dean/ Engineering Prof. L.L.Rathnayake.

I owe a debt of a gratitude to Head/ Mechanical Engineering, Dr. S.R. Tittagala who has provided feedback on early attempts, which has been incorporated to this successful one.

Thanks to all the current and former Supervisors of the project. In particular following individuals gave me their valuable advices and ideas in addition to proper guiding.

An extra special thanks goes to Dr. P.A.B.A. Ranjan Perera, a Supervisor of the Project, who after reading these chapters for several times an unerring eye for detail and manuscript editing support, must now know more than any other else.

Very special thanks go out to Dr. W.K. Wimalsiri, a Supervisor of the Project. His support continues to be invaluable appreciate the dedicated support of Dr. Wimalsiri, who provided ideas and advices through out the project.

Of course, Chairman/ Progress Review Committee Dr. Thusitha Sugathapala deserves special thanks for always keeping everything running smoothly and inspiring me when I didn't feel very inspired.

Thanks go to Mr. S.Ganesupiragash deciphering program properties and events in programming languages, providing useful suggestions.

I am specially appreciative the efforts of the Mr. Darshana Liyanage imparted to the hardware application.

Of course without the support of the staff in Maritime Division Mr. M.D.D. Gunathilake and Mr. Sunil Wickramasinghe, the Test Bed made for the project would be nothing more than a dream.



University of Moratuwa, Sri Lanka. Electronic Theses & Dissertations www.lib.mrt.ac.lk

				PAGE
LIST OF FIGURES A	ND TABLES			XIV - XX
LIST OF ABBREVIAT	TIONS			XXI - XXVIII
PREFACE .				xxix - xxxviii
	RATURE SURVEYS ITION MONITORING T DIAGNOSIS			1 - 13
I.I INTRODUC	TION			2
I . 2 PREVIOUS	LITERATURE REVIEWS	AND SURVEY	'S .	3
1.2.1	MASS UNBALANCE			6
1.2.2	BENT SHAFTS			8
1. 2. Unive	r GRACKEDISHAFTISIWA	, Sri Lanl	ca.	9
	ocan onecarrord Pla			9
1. 2. 5WWW.	WHAT IS CONDITION	MONITORING	'? .	10
1.2.6	WHERE CAN IT BE AP	PLIED .		10
1.3 LITERATU	RE SURVEY .			10
1.3.1	APPLICATION OF SHO (SPM) FOR ROLLING B DRAWBACKS AS A MO	EARING AND	ITS	10
1.3.2	DIFFERENCE BETWEE IBRATION	N SHOCK PUL	_SE AND .	II
1.3.3	PROCESSING SHOCK F	ULSE SIGNA	LS .	H
1.3.4	SHOCK PULSE PATTER	RNS .		12
1.3.5	MEASURING OPERATION	ON CONDITIO	N .	13
CHAPTER II CODE	ON NOISE LEVELS	ON BOARD	SHIPS	14 - 18
II . I SCOPE				15
II . 2 PURPOSE				15
II . 3 NOISE LEV	EL LIMITS .			15

Chapter III	CLAS	OR MECHANISMS IN SIFICATION; ELEMEN CES OF VIBRATION	•		19 - 20
III . I	CLASSIFI MECHANIS	ATION OF SHIPS ROTOR	. ,		20
III . 2	ELEMENT	S OF ROTOR MECHANISM	S IN SHIPS	•	20
Chapter IV	MODI	S OF VIBRATION			21 - 25
IV . I	TORSION	L VIBRATION .		•	22
ין	V . I . I	HOLZER ANALYSIS OF	TORSIONAL S	SYSTEM	23
1	V . 1 . 2	DRIVE TRAIN ANALYSIS	S .		23
l,	V . I . 3	VIBRATION AMPLITUDE	S .		24
IV . 2	RANDOM	IBRATION .		•	24
יו	V . 2 . I	WHY DO WE CARE ABO VIBRATION?	UT RANDOM		25
יו	V . 2 . 2	WHAT IS FREQUENCY F ANALYSIS ?	RESPONSE	٠	25
CHAPTER	EMAUN	ersity of Moratuwa CAUSTIQE SHIP MIB Hibamrt.ac.lk	BATIANIS		26 - 31 27
		THE ACTION OF THE S			27
		VIBRATION IN SHIPS			27
٧	'.1.3	OUT OF BALANCE FOR RECIPROCATING MACH			31
CHAPTER \	/I VIBR	ATION ANALYSIS			32 - 35
VI . I	INTRODUC	TION			33
VI . 2	ANALYSIS	FREQUENCY .			34
VI . 3	ADVANTA	GES / LIMITATIONS			35

CHAPTER VII FOL	JRIER ANALYSIS	36 - 7
VII . I CLASSIFI	CATION OF DATA	3 7
VII . I . I	DIFFERENCES BETWEEN DETERMINISTIC AND RANDOM DATA	37
VII . I . 2	STATIONARY AND ERGODIC RANDOM . DATA	38
VII . I . 3	NON-STATIONARY DATA	38
VII . I . 4	NATURE OF TRANSIENT DATA .	38
VII . I . 5	FREQUENCY SPACING AND LENGTH . CONSIDERATIONS	41
VII . I . 6	PADDING WITH ZEROS	42
VII . I . 7	EFFECT OF RECORD LENGTH	42
VII . I . 8	COMPUTATIONAL VERSUS RESOLUTION BANDWIDTH	43
VII . I . 9	RESOLUTION LIMITS	44
VII . I . 10	NONZERO MEAN VALUES	44
VII . I . II Unive	TIME WEIGHTING FUNCTIONS AND . erspectral Leakagea, Sri Lanka.	4 5
Asures	CANALYZING SHORT DURATION TRANSIENTS	45
VII . 1 . 113VW	LEFFECTS OF ZERO PADDING	46
VII . I . 14	EFFECTS OF RECORD LENGTH	46
VII . I . 15	EFFECTS OF TIME WEIGHTING FUNCTIONS . (WINDOWING)	46
VII . I . 16	HANDLING NON-ZERO MEAN VALUES .	47
VII . I . 17	PRACTICAL EXAMPLES USING . DETERMINISTIC AND RANDOM TRANSIENT WAVE FORM	47
VII . I . 18	CONTINUOUS SINE WAVE	50
VII . 2 THE COMP	PLEX FOURIER TRANSFORMS	54
VII . 2 . I	THE COMPLEX FOURIER TRANSFORMS . (IN DETAIL)	54
VII . 2 . 2	TIME AND FREQUENCY REPRESENTATION	55
VII . 2 . 3	TIME AND FREQUENCY DOMAINS .	55

	VII . 3	DISCRETE	FOURIER	TRANSFO	RM AND TH	IE FFT		59
	VII	. 3 . 1	INTRODUC	CTION			•	59
	VII	. 3 . 2	THE DISC	RETE FOU	RIER TRAN	SFORMS	S.	59
	VII	. 3 . 3	FAST FOL	JRIER TRA	NSFORMS			61
	VII	. 3 . 4	FILTERS					62
		VII. 3 .	4 . I F	LTERING				62
		VII.3	. 4 . 2 A	NTI-ALIAS	ING FILTE	RS		62
	VII	. 3 . 5	FOURIER	TRANSFOR	RM PROPER	TIES		65
		VII.3	. 5 . I S	CALING PR	OPERTY			65
		VII . 3	. 5 . 2 SI	HIFTING PI	ROPERTY	•		66
	VII	. 3 . 6		1ATION OF RMS WITH		ous		66
	VII . 4	SAMPLING	THEOREM					67
	VII . 5	REAL TIME	ANALYSIS	3 .				69
	VII . 6	C-PROGRAM	1 FOR FAS	T FOURIE	R TRANSF	ORMATIC	N	70
CHAI	PTERVI	Electron Rolling B	onic The	eses & T	wa, Sri I Dissertat			76 - 79 77
	VII	1.1.1			BEARINGS			78
	VII	1.1.2	SELF-ALI	GNING BAI	LL BEARIN	GS		78
	VII	1.1.3	ANGULAR	CONTACT	BALL BEA	ARINGS	•	78
	VII	1.1.4	NEEDLE F	ROLLER BE	ARINGS			78
	VII	1.1.5	SPHERICA	L ROLLER	BEARINGS	5		78
	VII	1.1.6	TAPER RO	OLLER BEA	ARINGS	•		78
	VII	1.1.7	THRUST E	BALL BEAF	RINGS			79
	VII	1. 1 . 8	CYLINDRI	CAL ROLLI	ER THRUST	T BEARIN	NGS	79
	VII	1.1.9	NEEDLE F	ROLLER TH	HRUST BEA	RINGS		79
	VIII . 2	HYDRO-DYN	IAMIC BEA	RINGS				79
	VIII . 3	SLEEVE BE	ARINGS					79

CHAPIER	LIFE	OF BEARING	5	•	•	•	80 - 87
IX . I	INTRODUCT	ION .					81
IX . 2	IRREGULAR	ITIES OF BALL	BEARING	S			82
IX . 3	BEARING W	EAR AND ITS (CAUSES .		•		83
IX	. 3 . 1	WEAR CAUSED	BY ABRA	SIVE P	PARTICL	ES	83
IX	. 3 . 2	WEAR CAUSED LUBRICATION	BY INADE	EQUAT	E		83
IX	. 3 . 3	WEAR CAUSED	BY VIBRA	NOITA			84
IX	. 3 . 4	SURFACE DIST	RESS AND) ITS (CAUSES		85
IX	. 3 . 5	IONS AND THE	IR CAUSE	S			85
IX .	3 . 6	INDENTATIONS MOUNTING OR			JLTY .		85
IX	. 3 . 7	DAMAGE CAUS ELECTRIC CUR		E PAS	SAGE O	F.	85
IX . 4	BEARING C	RACKS					86
IX	. 4 . 1	CRACKS CAUS	ED BY RO	UGH TI	REATME	NT	86
X	4 Unive	CRACKS CAUS	ED BY SM	EARING	anka.	•	86
	4 Electro	GRACKS GAUS	ER BY FR	PHINE	GORRO	OSION	86
IX . 5	BEARING	orrossion.lk					87
IX	. 5 . 1	CORROSION			•	•	87
IX	. 5 . 2	FRETTING CO	RROSION				87
CHAPTER X	VIBRA	TION MONIT	ORING .				88 - 91
Χ.Ι	INTRODUCT	ION .					89
X . 2	CORRECTIV	'E MEASURES					89
CHAPTER XI		TION MONIT		ND			92 - 100
XI . I		IONITORING SY ANCE PROCEDU	-		•	•	93
XI	. 1 . 1	PREDICTIVE M	AINTANA	NCE			93
XI	. 1 . 2	CONDITION MC	NITORING	;			94
XI . 2	FORMS OF	TECHNICAL MA	UNTANAN	CE			98
XI	. 2 . 1	METHODS FOR CONDITION OF				NISMS	98

CHAPTE	R XII VIBR	ATION M	EASURING	EQUIF	MENT		101 - 114
XII.I	INTRODUC	TION .					102
XII . 2	ACCELERO	METERS					104
	XII . 2 . I		OELECRIC E	FFECT,	THEORY,		104
XII . 3	CHARGE A	MPLIFIERS		•	•	•	109
	XII . 3 . I	TIME CON	NSTANT AND	DRIFT	,		110
	XII . 3 . 2	FREQUEN CONSIDER	ICY AND TIM RATION	IE DOMA	IN		110
XII . 4	LOW IMPED TRANSDUC		OELECTRIC	•	•		III
	XII . 4 . I	TIME CON	TNATE	•		•	112
XII.5	LOW IMPE	DANCE PO	WER SUPPLY	(COUPL	ER)		113
	XII . 5 . I	TIME CON	NSTANT	•	•		113
	XII . 5 . 2	SELECTIO	ON METRIX	•	,	•	113
	XII . 5 . 3	DUAL MO	DE CHARGE	AMPLIF	ERS	•	113
XII . 6	HIGH AND	LOW IMPE	DANCE SYST	E ^M Sri 1	Lanka.		114
	TOTAL CONTRACTOR OF THE PARTY O	onic The	eses & Di		tions		114
	XII . 6 . 2		EDANCE SYS	STEMS F	IIGH		114
	XII . 6 . 3	LOW IMPE	EDANCE SYS	STEMS		•	114
XII . 7	EXTERNAL	IMPEDAN	CE CONVERT	TERS			114
CHAPTER	XIII VIBRA	TION ME	ASURING	EQUIPN	MENT U	SED	115 - 119
XIII . I	PIEZOELEC	TRIC ACC	ELEROMETE	R, DESI	GN & USE		116
	XIII . I . I	MEASURII	NG ACCELER	RATION			116
	XIII . I . 2	ACCELER	OMETER MO	UNTING		•	118
	XIII . I	. 2 . I S	TUD MOUNT	ING			118
	XIII . I	. 2 . 2 A	DHESIVE MC	UNTING			118
	XIII . I	. 2 . 3 T	RIAXIAL MO	UNTING			119
	XIII . I	. 2 . 4 S	TRAIN RELIE	EVING C	ABLE		119
	XIII . I . 3	CALIBRAT	TION TECHN	IQUES			119
	XIII . I	. 3 . Г Д	CCELEROME	TERS			119

CHAPTER X	VIV VIBRATION MONITORING SYSTEM	120 - 124
XIV . I	INTRODUCTION	121
XIV . 2	WHY SEELVE BEARINGS ARE SELECTED ? .	123
XIV		123
XIV	V. 2. 2 OBSERVATIONS:	124
CHAPTER X	✓ DATA ACQUISITION CARD : ACL - 812PG	125 - 130
XV . I	INTRODUCTION	126
XV . 2	A SELECTION OF MEASUREMENT LOCATION .	127
XV . 3	SELECTION OF THE INTERVALS BETWEEN . MEASURMENTS	127
XV . 4	C-PROGRAME FOR CONVERSION OF ANALOG . SIGNAL INTO DIGITAL VALUES	127
XV . 5	PROJECT DATA	127
XV . 6	CONVERSION OF DIGITAL VALUE TO ACCELERATION UNITS	129
XV . 7	RESULTS OBTAINED FROM FAST FOURIER TRANSFORMATION F ACCEPARATIONS IN MARSEA.	130
	Electronic Theses & Dissertations	
CHAPTERX	VI WAUTOVIBRATION ANALYSING PROGRAMME	131 - 137
XVI.I	INTRODUCTION	132
XVI . 2	'AUTOVIB' - VIBRATION ANALYSING PROGRAMME .	135
XVI . 3	EXAMPLES OF GRAPHS OBTAINED FROM 'AUTOVIB' PROGRAM	135
XVII . 4	FAULT DETECTION IN ROTATING MACHINERY .	136
XVII . 5	OVERALL MEASUREMENT AND SPECTRUM . COMPARISION	136
XVII . 6	HOW SPECTRUM CHANGES ARE RELATED . TO THE CONDITION OF A MACHINE	136

CHAPTER XV	/II D	ATA ANA	LYSIS	•		•		138 - 168
E	ELECT	OPE SPEC RIC MOTO EMRI ANI	R	TAINED F	ROM			139
XVII . 2	COMPA AND AI		GRAPHS	S AL_BII,	AL_B2I		•	144
		AIN FAULT NE ROTAT				AT	•	146
XVII . 4 F	FINDIN	GS						165
CHAPTER XVI	III CC	NCLUSIO	NC			•		169 - 173
CONCLUSION	4		•	•	٠	•		170
APPENDIX - A		PROGRA RANSFOR		FAST	FOURIE	R.		174 - 177
APPENDIX - E		PROGRA IALOG S					ES	178 - 183
APPENDIX		iversity UTOVIB OGRAM w.lib.n			a Sri J ANALY sserta	l anka SING tions	· .	184 - 194
APPENDIX - E		TO SPEC						195 - 239
APPENDIX - E		IVELOPE ONDITION				RENT	•	240 - 285
APPENDIX - F	= VII	BRATION	I MONIT	FORING	TEST	BED		286 - 303
REFERENCES	5							304 - 311
GLOSSARY								312 - 320
GLOSSARY			•					313



LIST OF FIGURES

FIG NO.		FIGURE PA	PAGE NO		
FIG.	1.3.3.1	Shock Pulse Transducer and its Vibration Signal	П		
FIG.	1.3.4.1	Filtered Transducer Signals	12		
FIG.	1.3.5.1	Measurements using Shock Pulse Meter	13		
FIG.	11 . 1	Allowable Daily and Occasional Noise Exposure Zones	16		
FIG.	11 . 2	Resonance Curve	17		
FIG.		ไรเล่ะเราอ่ยุง คนิโล Oratuwa, Sri Lanka. Electronic Theses & Dissertations	44		
FIG.	VII . 1 . 17 . 1	www.lib.mrt.ac.lk Half Cycle Sine Pulse, Its Fourier Transform Magnitude, and Imaginary Component (scale shifted).	48		
FIG.	VII . I . 17 . 2	One Cycle Sine Pulse, and Its Fourier Transform Magnitude.	49		
FIG.	VII . I . 17 . 3	5 Sine Wave and Its Fourier Transformation Curves	51		
FIG.	VII . I . 17 . 4	Fourier Transform of 1Hz	53		
FIG.	VII . 2 . 3 . I	Time Domain Signal	56		
FIG.	VII . 2 . 3 . 2	Prequency Domain	56		
FIG.	VII . 2 . 3 . 3	5 Example of a Non - Harmonic Periodic Motion (Piston Acceleration of a Combustion Engine)	57		
FIG.	VII . 2 . 3 . 4	Illustration of How the Waveform can be "Broken Up" into a Sum of Harmonically Related Sine-Waves	57		

FIG. VII . 2 . 3 . 5	Illustration of How the Signal can be Described in Terms of a Frequency Spectrum	58
FIG. VII . 4 . I	Undersampled, Oversampled, and Critically -Sampled Unit Area Gaussian Curves.	68
FIG. VII . 6 . I	Recording an Array (Here of Length 8) by Bit Reversal, (A) between Two Arrays, versus (B) In Place.	73
FIG. VII . 6 . 2	Input and Output Arrays for FFT	75
FIG. XI . 2 . I . I	Measured Vibration from Tests of Periodic Conditions	99
FIG. XI . 2 . I . 2	A Typical Model of a Mechanism, in Absence of	99
	Prophylactic Maintenance	
FIG. XII . 2 . I . I	Thin Slab Representation of Crystals	106
FIG. XII . 2 . I . 2	Various Effects on Crystals	106
FIG. XII . 2 . I. 3	Typical Frequency Response Curve	108
FIG. XII . 3	Simplified Charge Amplifier Model	109
	Flectronic Theses & Dissertations PIEZOTRON Circuit & Coupler www.lib.mrt.ac.lk	Ш
FIG. XIII . I . I . I	Typical Compression Mode Accelerometer	116
FIG. XIII . I . I . 2	K-SHEAR Accelerometer	117
FIG. XIII . I . 2 . 4	. I Cable Strain Relief	119
FIG. XIV . I . I	Vibration Monitoring System	122
FIG. XIV . 2 . I . I	Sleeve Bearing Assembly	123
FIG. XIV . 2 . I . 2	Ball Bearing Assembly	123
FIG. XVI . I . I	Illustrating of View Ports	134
FIG. XVI . 3 . I	Example of Graph Obtained from `AUTOVIB' Program	135
FIG. XVI . 3 . 2	Example of Graph Obtained from `AUTOVIB' Program	135
FIG. XVII . I . I	Characteristics of Electric Motor with No Speed	140
FIG. XVII . I . 2	Characteristics of Electric Motor in Running	142

FIG.	XVII . I . 3	Characteristics of Electric Motor with Coupling attached	143
FIG.	XVII . 2 . I	Characteristics of Aligned Shaft - Vibration Measured on First Bearing	145
FIG.	XVII . 2 . 2	Characteristics of Aligned Shaft - Vibration Measured on Second Bearing	145
FIG.	XVII . 2 . 3	Characteristics of Aligned Shaft - Vibration Measured on Third Bearing	146
FIG.	XVII . 3 . I	Characteristics of Bearing No. 1 with Loosen Coupling No. 1	147
FIG.	XVII . 3 . 2	Characteristics of Electric Motor with Loosen Coupling No. 2	148
FIG.	XVII . 3 . 3	Characteristics of Bearing No. 2 with Loosen Coupling No. 1	149
FIG.	XVII . 5. 4	Characteristics of Bearing NS 13 Lwith Leosen ESeupling NS 12eses & Dissertations	150
FIG.	XVII . 3 . 5	www.lib.mrt.ac.lk Typical Spectrum – Summary of Graphs XVII . 3 . 2, 3 and 4	150
FIG.	XVII . 3 . 6	Characteristics of Bearing No. 1 without Lubrication	151
FIG.	XVII . 3 . 7	Characteristics of Bearing No. 2 without Lubrication	152
FIG.	XVII . 3 . 8	Characteristics of Bearing No. 3 without Lubrication	153
FIG.	XVII . 3 . 9	Typical Spectrum - Summary of the Graphs made Out of FIG. XVII . 3 . 6, 7 and 8	153
FIG.	XVII . 3 . 10	Characteristics of Bearing No. 1 with Loosen	154

FIG. XVII . 3 . II	Characteristics of Bearing No. 2 with Loosen Coupling No. 2	154
FIG. XVII . 3 . 12	Characteristics of Electric Motor with Loosen Coupling No. 2	155
FIG. XVII . 3 . 13	Characteristics of Bearing No. 1 with Loosen Bearing No. 1	156
FIG. XVII . 3 . 14	Characteristics of Bearing No. 1 with Loosen Bearing No. 2	157
FIG. XVII . 3 . 15	Characteristics of Bearing No. 1 with Loosen Bearing No. 3	158
FIG. XVII . 3 . 16	Effects of Soft Foot	158
FIG. XVII . 3 . 17	Characteristics of Bearing No. 1 with Loosen Cap No. 1	159
	Characteristics of Bearing No.13 with Leosen Esection Theses & Dissertations	160
FIG. XVII . 3 . 19	www.lib.mrt.ac.lk Characteristics of Electric Motor with Loosen Cap No. 1	160
FIG. XVII . 3 . 20	Characteristics of Electric Motor with Loosen Cap No. 2	161
FIG. XVII . 3 . 21	Characteristics of Bearing No. 1 with Loosen Cap No. 2	161
FIG. XVII . 3 . 22	Characteristics of Bearing No. 2 with Loosen Cap No. 2	162
FIG. XVII . 3 . 23	Characteristics of Bearing No. 1 with Loosen Cap No. 3	162
FIG. XVII . 3 . 24	Characteristics of Bearing No. 2 with Loosen	163

FIG. XVII . 3 . 25	Cap No. 3	163
FIG. XVII . 3 . 26	Characteristics of Electric Motor with Loosen Cap No. 3	164
FIG. XVII . 3 . 27	Typical Spectrum - Summary of the Graphs made Out of FIG. XVII . 3 . 18,19,20,21,22 and 23	164



LIST OF TABLES

TABLE NO.	TABLE	PAGE NO
TABLE VII . I . 4 . I	BASIC FORMS OF FOURIER TRANSFOME	40
TABLE VII . 3 . 4 . 2 . I	SYMMETRY PROPERTIES OF THE FOURIER TRANSFORM	64
TABLE XI . I . 2 . I	MONITORING PARAMETERS	97
(Electr	rsity of thostained Stitem analog onic /Digital Convension is lib.mrt.ac.lk	G 128
TABLE XV . 7 . I	RESULTS OBTAINED FROM FAST FOURIER TRANSFORMATION	Γ 130



CHAPTER I

dBsv Decibel shock value

dBi Initial shock value

dB_N Normalized shock value

CHAPTER II

v impact velocity

dB(A) Vibration energy measurement

L Length of the structure

M Function of the mass at the structure and its distribution

Second moment of area of the material of the structure

about its neutral axis.

f Urrequenciy of applied forceva, Sri Lanka.

fn Frequency of Natural Structure entations

www.lib.mrt.ac.lk

CHAPTER IV

m	Mass or inertia (in	Spring-mass system) (kg)
***	TITADO OF THEFT IN	. Spring mass by sterm, (Rg.)

J Mass or inertia (in Torsional system) (kg m²)

K_m Spring (in Spring-mass system) (Nm)

K_T Spring (in Torsional system) (Nm/rad)

c_m Damping (in Spring-mass system) (Ns/m)

c_T Damping (in Torsional system) (Nms/rad)

a Acceleration (in Spring-mass system) (m/s²)

 \ddot{o} Acceleration (in Torsional system) (rad/s²)

v Velocity (in Spring-mass system) (m/s)

ò Velocity (in Torsional system) (rad/s)

y Displacement (in Spring-mass system) (m)

θ Displacement (in Torsional system) (rad)

CHAPTER VII

F	(t)	Fourier	Transform _	Time resu	ponse function
1	(1)	rounci	Transform –	1 11116 162	ponse function

TPeriodic time

 ω_T Angular velocity

Time

 a_0, a_n, b_n Fourier transform coefficients

Integral multiplier n

Fundamental frequency (first harmonic) f_0

 Δf Frequency interval

Fourier time response f(t)

Number of discrete values N

Sampling interval Δt

Sampling rate f_{s}

Nyquist frequency f_{Nv}

Fourier Transform of Frequency response function F(f)

Electronic Theses & Dissertations
Boxcar time response function

 $U_{I\!R}(f)$ Boxcar frequency response function

 ΔN Number of padded zeros

M'Number of data values in time series

Frequency Increment Δf¨

 B_e Resolution bandwidth

 f_{max} Highest frequency

 $X_{(l)}$ Fourier transform

Inverse fourier transform $X_{(t)}$

k Integral coefficient

Fourier transform coefficients a_k, b_k

Original functions $f_{(x)}$, $g_{(x)}$

Function after convolution $F_{(s)}$, $G_{(s)}$

X(mF)Discrete frequency transform function

x(nT)	Time response function
realOut	Array of coefficients of cosine waves in the Fourier formula.
imagOut	Array of coefficients of sine waves in the Fourier formula.
h(t)	Impulse response
x(t)	Input time domain
y(t)	Output time domain
X(f)	Input frequency domain
Y(f)	Output frequency domain
H <i>(f)</i>	Impulse frequency domain
f(w)	Fourier transform function
f(x)	Continuous time function
E(x)	Even part of function $f(x)$
O(x)	Odd part of function $f(x)$
f*(-x)	Umaginary function ratuwa, Sri Lanka.
F*(-s)	Elemplex Conjugate of Function f(x) ions
F(s)	www.lib.mrt.ac.lk Fourier Transform function of f(x)
\wp_c	Cosine Transform
\$0 s	Sine Transform
i	Numerous
x_{θ}	A Real constant
β	$= (x - x_0)$
В	A frequency in Hz
H_n	Discrete Fourier transform of N-points
W	A Complex Number
h_k	A Vector
F_k	k th component of fourier transform
F^e_{k}	$k^{\prime h}$ Component of Fourier transform of length $n/2$
data[1]	Real part of f_0
data[2]	Imaginary part of f_0

CHAPTER IX

 L_{10} Basic rating life of bearing

CHAPTER XII

f_n Undamped natural (resonant) frequency (Hz)

f Frequency at any given point of the curve (Hz)

a_o Output acceleration

a_b Mounting base or reference acceleration

Q Factor of amplitude increase at resonance

C_t Transducer capacitance

C_c Cable capacitance

C_r Range (or feedback) capacitor

R_t Time constant resistor (or insulation of range capacitor)

R_i Insulation resistance of input circuit (cable and transducer)

q Charge generated by the transducer Lanka.

V_o Eductions de Dissertations

A www.lib.mrt.ac.lk

TC Time Constant

q Charge generated by piezoelectric element

V_i Input signal at gate

C_q Transducer capacitance

C_G MOSFET GATE capacitance

CHAPTER XIII

F Force

m Mass

a Acceleration

CHAPTER XIV

T1, T2, T3 Accelerometers

EM Electric motor

B1, B2, B3 Bearings

TS Tail shaft

IS Intermediate shaft

C1, C2 Couplings

CHAPTER XVII

N Motor speed (rps)

n Number of balls

d Ball diameter

D Pitch diameter

B Contact angle of ball

Z University of Moratuwa, Sri Lanka.
Number of polls
Electronic Theses & Dissertations

F_L Vine frequency ac. 1k

N_s Synchronous speed

F_{rot} Rotational frequency

F_s Slip frequency

F_p Pole frequency

F_z Slot frequency

 $F_z \pm F_{rot}$ Side bands

 F_z -2 $F_L \pm F_{rot}$ Side bands

F_m Main supply frequency

EMO Characteristics of electric motor at 0 rpm

ECUP Characteristics of electric motor running with attached coupling

only

EMR Characteristics of electric motor running with shafting and

propeller

CAP1_B11	Characteristics of bearing no. 1 with loosen cap no.1
CAP1_B21	Characteristics of bearing no. 2 with loosen cap no.1
CAP1_B31	Characteristics of bearing no. 3 with loosen cap no.1
CAP1_EM1	Characteristics of electric motor with loosen cap no.1
CAP2_B11	Characteristics of bearing no. 1 with loosen cap no.2
CAP2_B21	Characteristics of bearing no. 2 with loosen cap no.2
CAP2_B31	Characteristics of bearing no. 3 with loosen cap no.2
CAP2_EM1	Characteristics of electric motor with loosen cap no.2
CAP3_B11	Characteristics of bearing no. 1 with loosen cap no.3
CAP3_B21	Characteristics of bearing no. 2 with loosen cap no.3
CAP3_B31	Characteristics of bearing no. 3 with loosen cap no.3
CAP3_EM1	Characteristics of electric motor with loosen cap no.3
LB1_B11	Characteristics of bearing no. 1 with loosen bearing no.1
LB1_B21	Characteristics of bearing no. 2 with loosen bearing no.1
LB1_B31	Characteristics of bearing no. 3 with loosen bearing no. 1
LB1_EM1	Characteristics of electric motor with loosen bearing no. l
LB2_B11	Characteristics of bearing no. 1 with loosen bearing no.2
LB2_B21	Characteristics of bearing no. 2 with loosen bearing no.2
LB2_B31	Characteristics of bearing no. 3 with loosen bearing no.2
LB2_EM1	Characteristics of electric motor with loosen bearing no.2
LB3_B11	Characteristics of bearing no. 1 with loosen bearing no.3
LB3_B21	Characteristics of bearing no. 2 with loosen bearing no.3
LB3_B31	Characteristics of bearing no. 3 with loosen bearing no.3
LB3_EM1	Characteristics of electric motor with loosen bearing no.3
LC1_B11	Characteristics of bearing no. 1 with loosen coupling no.1
LC1_B21	Characteristics of bearing no. 2 with loosen coupling no.1
LC1_B31	Characteristics of bearing no. 3 with loosen coupling no.1
LC1_EM1	Characteristics of electric motor with loosen coupling no.1
LC2_B11	Characteristics of bearing no. 1 with loosen coupling no.2
LC2_B21	Characteristics of bearing no. 2 with loosen coupling no.2

LC2_B31	Characteristics of bearing no. 3 with loosen coupling no.2
LC2_EM1	Characteristics of electric motor with loosen coupling no.2
UM_B11	Characteristics of bearing no. 1 with unbalance mass
UM_B21	Characteristics of bearing no. 2 with unbalance mass
UM_B31	Characteristics of bearing no. 3 with unbalance mass
UM_EM1	Characteristics of electric motor with unbalance mass
NOL1_B11	Characteristics of bearing no. 1 without lubrication
NOL2_B21	Characteristics of bearing no. 2 without lubrication
NOL3_B31	Characteristics of bearing no. 3 without lubrication
ECUP	Characteristics of electric motor with coupling attached
AL_B11	Characteristics of bearing no. 1 with shaft aligned
AL_B21	Characteristics of bearing no. 2 with shaft aligned
AL_B31	Characteristics of bearing no. 3 with shaft aligned



PREFACE University of Moratuwa, Sri Lanka.



University of Moratuwa, Sri Lanka. Electronic Theses & Dissertations www.lib.mrt.ac.lk

PREFACE

A ship is the home of the crew for months at a time and of her passengers perhaps for weeks. The influence of vibration upon comfort is therefore extremely important and will be a factor in the reputation of any passenger ship.

Vibration Problems on ships such as mast, foundation, and propeller shaft vibration excited by propulsion system frequencies can lead to structural fatigue, damage to machinery, and can be annoying, uncomfortable, and dangerous for persons on the ship.

Vibration has been a matter of concern to ship designers since the end of the 19th century although its presence in ship characteristics was known long before that time and its importance has become much emphasized over the last half century. Some sailing warships, particularly the lightly-built frigates, suffered from serious vibration aft when driven hard, probably as a result of flow interaction while there are accounts of mast/sail combinations causing such severe vibration that crewmen were thrown from their feet or, worse, from their mast-top positions.

Today, an increasing number of new or alternative ships is launched - very large and very fast container ships, cruise ships, tankers with modern propulsion systems. Due to little experience with such ships, living conditions can be adversely affected by vibration if the frequencies of major excitations are close to a natural frequency of the superstructure or a part of it.

In ships, there are so many sources of noise and Vibration such as propulsion engines and electric generators in restricted spaces and structures of ships, which are made of steel, transmit vibration well. By the reasons, noise and vibration of ships are very big by nature and reduction of noise and vibration is important subject for ships.

Effect of Vibration:

One can distinguish two areas, where standards have been developed to assess the effect of vibration, applied to the human body: vibration passing to hand and whole body. The vibration passes to hand, can cause the disease, called as "white finger disease," the latter can lead to variety of health problems, ranging from motion sickness to tissue damages. It should be noted, that the relationship between exposure and the disease is complex and many questions in this area, remain unanswered. A number of standards incorporating the latest state of knowledge have been introduced over the last few years with the object of giving guidance to those, who required to assess the importance of human vibration exposure.

It is now generally believed that vibration causes damage to blood vessels, which are thus made incapable of circulating blood to the extremities. There is no known cure and symptoms, which are irreversible. So it is clearly important to establish the levels of vibration and the duration of exposure, which are statically likely to cause the disease and to take precautions.

www.lib.mrt.ac.lk

Noise:

Noise has been recognized as a nuisance (in the legal sense) for many years. Nuisance can be either public or private. A private nuisance is commonly defined as an unlawful interference with a person's use or enjoyment of land or of some right over it or in connection with it. A public noise is an unlawful act or omission causing interference with the health and safety of the public at large. A noisy operation can be both a public and a private nuisance. It is not always easy to answer the question of whether the nuisance complained of is a public or a private one. If the noise nuisance affects just one person or a household, it is clearly a private nuisance. If it affects a class of the public, such as the residents of a community or of the passers-by of a noisy factory, it is likely to be a public nuisance.

A private action can only be brought by the occupier of the land or by someone who has a legal interest in the land, and he can only take action against the person who cause the nuisance. A public nuisance is a crime, and proceedings can be taken by public bodies such as the local authority or Attorney-General or both. All the criminal sanctions are available to the court, an in addition it has power to issue an abatement order, which may take the form of restricting the noise to certain hours, or levels, or to cease entirely.

It is well known that much of modern technology is derived from projects ordered by the military industry of the developed countries. The deepest research of machines and equipment vibration is done initially in countries with strong naval forces, which have important needs to minimize noise and vibration. A number of naval research centers that deal with using and developing analytical tools for vibration measurement and reduction exist in Countries. These Developed centers are equipped with instrumentation for measurement and analysis of signals ,mostly using instruments produced by Bruel & Kjaer (Denmark) and Kistler (Norway). A University of Moratuwa, Sri Lanka. number of highly qualified experts work in these centers and prepare specialists for navy and shipbuilding industry.

The greatest advances can make in the condition diagnostics of machines using vibration., The AUTOVIB monitoring method for condition diagnostics of machines using vibration can be successfully used in a number of civil industries including energy, nuclear power plants, paper and pulp, metallurgy, transport including ships, aviation and railways.

One of the main problems in Sri lanka is a great shortage of specialists who can efficiently use condition monitoring and diagnostics systems, including those with expert systems that are supplied by the leading Western companies. To prepare these specialists would take too much time. This fact has defined the main peculiarities of the vibration diagnostics in Sri lanka. The strategy of AUTOVIB, is to develop a system for condition diagnostics of sleeve bearings (fluid film bearings) that can be applied equally for ball bearings as well.

The main problems peculiar to the Sri lankan market

The changes associated with the introduction of market relations in the number of industries in Sri lanka were started at the end of the 1956 and after 1980s with the introduction of Open economy. Plans for restructuring the economy included plans to decrease production costs and excess labour energy. The drawbacks prevail in improving of the efficiency of production processes is based on three main assumptions:

- The absence of financial resources in the country to renew the machinery
 and equipment in the majority of industries for at least five to ten years.
 The natural wear of the equipment should significantly increase its
 maintenance costs and the introduction of the condition diagnostics
 systems is likely to be the most practical way to decrease these costs.
- Relatively high investments over high level diagnostic systems (Automatic Condition monitoring Systems) prevent owners by utilizing such a system.
- Significant limitations of existing condition diagnostic technologies from leading Western companies.
 Intersity of Moratuwa, Sri Lanka.

The following reasons that limit the use of modern condition monitoring and diagnostics systems of American and West-European production in Sri lanka

- The absence in most regions of qualified personnel who can use these systems, despite the existence of a number of scientific centers with experts of higher qualification. The problem is that to prepare a person to be a qualified expert takes several years and would require significant financial resources.
- The high relative price of the common monitoring and diagnostic systems in Importing. For example, in the West the price of the diagnostic instrumentation needed for an expert to work on the enterprise is less than or equal to compared to the labor costs of an expert for the enterprise during a year. In Sri lanka, taking into account the tax policy, the price for the diagnostic equipment equals the income of an expert for about ten years. This makes the survival of small companies specialized in diagnostic services impossible.

- One more reason, which is also economic is the high costs of mounting permanent transducers on existing equipment. Typically, the construction of units should be redesigned to assure appropriate mounting and protection of the transducers so as not to destroy them in the process of standard maintenance of the equipment.
- The last reason is connected to the existence of various standards and regulations that differ in each industry that define the requirements for different parameters of the main equipment and methods for their control. These regulations do not allow making a decision for maintenance and repair of the equipment without conducting standard measurements that usually require the shutdown of the equipment and partial disassembly of the units. That's why these regulations make it impossible to use modern condition monitoring systems and use condition based maintenance.

This analysis of the current situation led to a recommendation to speed up the development of the methods for mass condition diagnostics that can be carried out by a user with no special training in condition diagnostics. These methods were developed over a period of several years based on the analysis of machine vibrations in the shipbuilding industry and the resultant extraction of diagnostic information signals. The methods developed were intended to be used for condition diagnostics of supplementary machines and equipment the maintenance of which was not governed by the existing standards and regulations.

This analysis was the base of this project. At the same time, a number of problems became evident during the detailed market research stage:

 The first problem was the need for application software based on the developed methods that would efficiently replace a qualified expert. The system should ask the customer to describe the equipment for diagnostics, define what data should be measured, process the measured data, make condition diagnostic and prediction for the machines and equipment under control. The second problem occurred after the start of the exploitation by the
customers of the automatic diagnostic systems consisting of the
measurement device, personal computer and the application software.
This was the problem of the customers support in those rare situations
when the automatic diagnostics did not answered the question of what is
the defect in the machine and how dangerous it is.

Noise Generated From Machine Vibrations

If you want to reduce maintenance costs you must improve equipment maintainability and reliability. The premise being, if the equipment does not fail as often, it costs less to repair. When equipment does fail, longer life can be achieved if proper repairs are made. Proper repairs means the cause of failure must be identified and eliminated. If this is not done the equipment will fail again. These objectives can be accomplished during the acquisition phase of new equipment, the purchase of spare parts, and accurate diagnosis of all rotating machinery problems. If either of these items are not properly managed the objectives may not be achieved to evaluations, payment of bonuses; production objectives and other brownie point systems tend to focus management's attention on the short term instead of the long term. This can also affect maintainability and reliability.

In field balancing machines with high vibrations, the use of common methods of determining balance weights often does not yield satisfactory results. An analysis of the reasons for this shows that there are two main groups of constraints on the balancing efficiency: The forces of different nature from simple unbalance that excite vibration at the rotating frequency and the existence of certain defects in the machine that can change the mechanical properties of the machine.

The technology on how to diagnose problems in rotating machinery is equally unparalleled. The technology has progressed from amplitude measuring and trending to using the time domain signal, phase, and frequency domain spectra for accurate diagnosis of specific problems. In fact, it may be time to



progress to the next step beyond predictive maintenance to equipment maintainability and reliability.

Consideration of the reliability and service life of a machine suggests that low frequency vibrations present the greatest source of danger to a machine. For machines with rotating parts (rotors), this is typically a vibration at the rotation frequency. This vibration may significantly increase during the machine operation. Usually, when the vibration level exceeds certain limits, the users conduct maintenance of the machine. The inertial forces due to the unbalance of the rotating parts relative to the rotation axis are typically considered to be the reasons for the vibration increase. That's why the users try field balancing the machine when possible. Unfortunately, attempting to balance the machine may not always produce acceptable results. The main reasons for this are other problems of the machine or of its supports. To eliminate additional expenses and delays, the customer should have the information about the various possible defects of the machine that can be responsible for the machine vibration at the rotating frequency and this information should be available before or at least during frequency and this information should be available before or at least during frequency and this information should be available before or at least during these and this information.

The factor, the vibration still remains as an actual problem with increase in speed and load of machines in ships. The technical diagnostic is the process of testing the machine, in order to test the condition of it. Therefore the technical diagnostic helps to detect the faults of machines while they operate. The change in condition of vibration of machines may cause the change in technical condition of ship machinery then the condition of the ship.

The term **Diagnostic** is a Greek word, and means the ability to discern. It is used in Medical Science. That is the section, which indicates the symptoms of diseases and methods using to identify the diseases.

Accurate Diagnosis

Accurate diagnosis of machinery problems provides the intelligence for new equipment acquisitions, spare parts purchasing, and necessary repairs. This is why this very important function must be part of the Equipment Maintainability and Reliability group.

Once a problem has been identified the necessary maintenance and engineering talent must be available to determine the proper fix. Accurate diagnosis of machinery problems requires a lot more than condition monitoring and trending. Accurate diagnosis requires the proper hardware, software, technology, and skilled people. This includes the use of frequency domain spectra, time domain signals, and phase relationships of frequencies. The first response is "we can't afford that." The fact is that you can't afford not to do accurate diagnosis.

If the right hardware, software, and technology are placed in the hands of skilled people, the payback period is the shortest, and the return on investment (ROI) is more than for any other investment today. These savings are realized by a reduction in maintenance cost and increased production. Managers should realize they may have to purchase new equipment analyzers and transducers. High quality personnel should be assigned to the program. These people must be trained in the best technology. People's attitude should be changed from condition monitoring and trending to accurate diagnosis with vibration analysis. If these objectives are achieved, the increase in profits for a medium plant should be at least one million dollars per year.

Imbalance is a linear problem. Linear problems behave in a linear manner. If a machine is out of balance, you should be able to balance it in three or four runs. If balancing is so simple, what is the problem? The problem is inaccurate diagnosis. There are a lot of vibration "experts" that cannot tell the difference between imbalance, looseness, bent shaft, misalignment, softfoot, broken rotor bars, and loading. All of these problems can cause a high amplitude at rotor speed, however these problems cannot be solved by balancing.

The program "AUTOVIB" gives a broad range of options to diagnose above mentioned disorders and irregularities of the machinery.

